

**CERAMICS ON THE BASIS OF NANODISPERSE SILICON  
NITRIDE PREPARED AT 1850 °C BY HOT PRESSING****UZ SILĪCIJA NITRĪDA NANOPULVERU BĀZES AR KARSTO  
PRESĒŠANU 1850 °C TEMPERATŪRĀ IEGŪTĀ KERAMIKA**

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**Introduction**

According to [1] there are two approaches to improve the mechanical properties of ceramics: one is the control of microstructure and another is the fabrication of composite. The microstructure of material can be significantly changed, by using nanosized compounds and their composites for preparation of materials. The distinctive properties of nanophase materials are low temperature plasticity, high diffusion coefficient and high solubility. Owing to good corrosion resistance and mechanical characteristics silicon nitride based ceramics are promising candidate for structural materials [2]. However, its use has been limited by its relatively low fracture toughness and the fact that its mechanical properties degrade at temperatures above 1200 °C. As it was shown in research [3], if nanosized Si<sub>3</sub>N<sub>4</sub> powders and composites (Si<sub>3</sub>N<sub>4</sub>-Me<sub>2</sub>O<sub>3</sub>, Si<sub>3</sub>N<sub>4</sub>-SiC) are used, high mechanical properties remain up to 1400 °C and higher temperatures.

It is well known that properties of silicon nitride ceramics could be increased by addition of a second nano-phase. Flexural strengths of up to 1,5 GPa were attained for material  $\text{Si}_3\text{N}_4$ -25 vol.% SiC, while the hardness increased to 19 GPa from 15 GPa for monolithic  $\text{Si}_3\text{N}_4$  [4]. Advantages of  $\text{Si}_3\text{N}_4$ -TiN composite powders have been described in [1].

Ceramic materials on the basis of silicon nitride are widely used in different fields, including cutting tools and high temperature construction materials for application at temperatures up to 1400 – 1500 °C in motor works, aircraft and aerospace (details of internal-combustion engines and gas-turbines, ball and sliding-bearings for exploitation at the extreme conditions etc.) [5].

Therefore, the aim of this investigation was to compare sintering, microstructure and properties of nanosized  $\text{Si}_3\text{N}_4$ - $\text{Me}_2\text{O}_3$  composite powder and its mixture with the second phase by means of hot pressing at 1850 °C as a compacting method.  $\text{Si}_3\text{N}_4$ -6 $\text{Y}_2\text{O}_3$ -3 $\text{Al}_2\text{O}_3$  was used as a basic powder and its mechanic mixtures with other nanopowders ( $\text{Si}_3\text{N}_4$ -SiC,  $\text{ZrO}_2$ , TiN) as well as composite powder  $\text{Si}_3\text{N}_4$ -TiN.

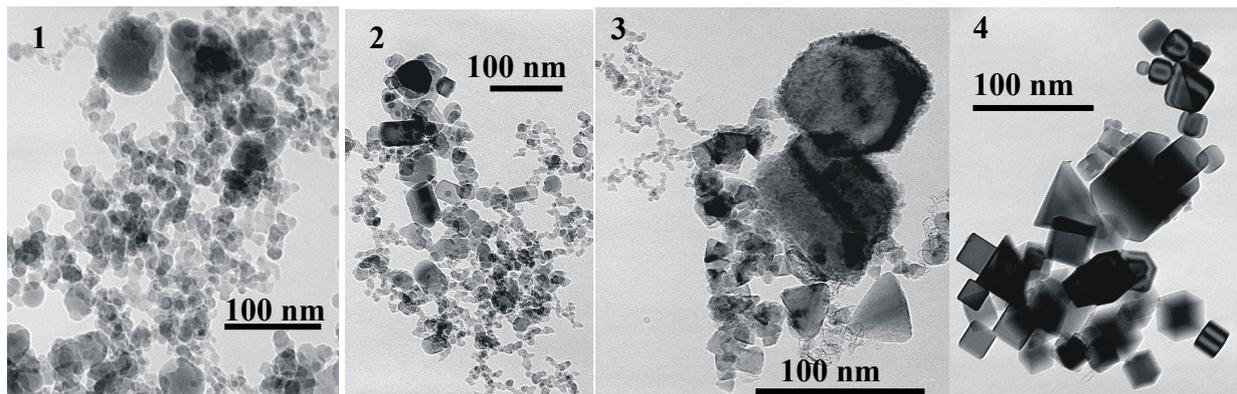
## Experimental

Fine powders of  $\text{Si}_3\text{N}_4$ -6 $\text{Y}_2\text{O}_3$ -3 $\text{Al}_2\text{O}_3$ -,  $\text{Si}_3\text{N}_4$ -TiN- system as well as dopants ( $\text{Si}_3\text{N}_4$ -SiC,  $\text{ZrO}_2$ , TiN) were formed by the plasma chemical synthesis method [6]. Chemical content of products is given in the Table 1.

The average particle size of the nanosized composites is in the range of 30-60 nm (Fig. 1). The  $\text{Si}_3\text{N}_4$ -6 $\text{Y}_2\text{O}_3$ -3 $\text{Al}_2\text{O}_3$  powders have irregular shape. The plasma produced  $\text{Si}_3\text{N}_4$ -TiN and  $\text{Si}_3\text{N}_4$ -SiC consists from TiN and SiC powders coated with layer of  $\text{Si}_3\text{N}_4$ .

**Table 1.**  
Chemical and phase composition and size distribution of used nanosized powders

The used powders	Chemical composition									Phase composition	SSA, m <sup>2</sup> /g	d <sub>50</sub> , nm
	Si	Y	Al	Zr	Ti	Si <sub>free</sub>	N	C	O			
$\text{Si}_3\text{N}_4$ -6 $\text{Y}_2\text{O}_3$ -3 $\text{Al}_2\text{O}_3$	53,2	4,8	1,5	-	-	0,6	35,3	-	4,6	crystallinity 20%; $\alpha/\beta \approx 1$	65	35
$\text{Si}_3\text{N}_4$ -TiN	52,8	-	-	-	7,5	0,7	37,2	-	2,3	amorphous $\text{Si}_3\text{N}_4$ , weak TiN	60	40
$\text{Si}_3\text{N}_4$ -SiC	66,7	-	-	-	-	0,8	4,2	26,2	2,0	$\beta$ -SiC; amorphous $\text{Si}_3\text{N}_4$	36	60
$\text{ZrO}_2$	-	-	-	73,8	-	-	0,5	-	25,7	70% teragon., 30% monoclin.	30	40
TiN	-	-	-	-	77,1	-	22,3	-	1,8	TiN cubic	40	30



**Fig. 1.** Characteristic shape of particles of used nanopowders:  
 1 -  $\text{Si}_3\text{N}_4\text{-}6\text{Y}_2\text{O}_3\text{-}3\text{Al}_2\text{O}_3$ ; 2 -  $\text{Si}_3\text{N}_4\text{-TiN}$ ; 3 -  $\text{Si}_3\text{N}_4\text{-}80 \text{ wt. } \% \text{ SiC}$ ; 4 -  $\text{TiN}$ .

Characteristic feature of plasmachemical nanosized powders are low degree of crystallinity. The degree of crystallinity of  $\text{Si}_3\text{N}_4$  in the  $\text{Si}_3\text{N}_4\text{-}6\text{Y}_2\text{O}_3\text{-}3\text{Al}_2\text{O}_3$  and  $\text{Si}_3\text{N}_4\text{-TiN}$  systems reaches only 20% and ratio of  $\alpha/\beta\text{-Si}_3\text{N}_4$  is close to one. The presence of oxide phases has not observed. In the  $\text{Si}_3\text{N}_4\text{-SiC}$  system the silicon nitride is X-ray amorphous, but silicon carbide is presented by well crystalline  $\beta\text{-SiC}$ .

Starting  $\text{Si}_3\text{N}_4\text{-}6\text{Y}_2\text{O}_3\text{-}3\text{Al}_2\text{O}_3$  composite powders were mixed with 10 wt. % of second nanophase ( $\text{Si}_3\text{N}_4\text{-SiC}$ ,  $\text{ZrO}_2$ ,  $\text{TiN}$ ) and mixed for 15 hours in ball mills. Polyethylene vessels and silicon nitride grinding balls were used. Isopropyl alcohol was used as a dispersion medium. After mixing, the sample was treated for 1 h with ultrasound and mixed additionally for 2 h in ball mills. The starting powder ( $\text{Si}_3\text{N}_4\text{-}6\%\text{Y}_2\text{O}_3\text{-}3\%\text{Al}_2\text{O}_3$ ), as well as the mixture of plasma prepared  $\text{Si}_3\text{N}_4\text{-TiN}$  nanocomposite with 3 wt. % of  $\text{Al}_2\text{O}_3$  (“Alcoa”) and 6 wt. % of  $\text{Y}_2\text{O}_3$  (“Nanophase”) were prepared in the similar way.

The obtained mass was dried at 80 °C and sieved through a 200  $\mu\text{m}$  sieve. Prepared powders were compacted by hot pressing at 1850 °C for 2 hours in nitrogen. The loading pressure was 30 MPa and temperature rising rate was 10°/min. All powders were sintered under the same conditions.

Discs with the diameter of 65 mm and 6 mm of height were obtained, from which bars of size 5x5x45 mm were cut for bend strength investigations.

Chemical composition of powders (N, C,  $\text{Si}_{\text{free}}$ , Y, Al, Ti) was determined by chemical analysis. Particle morphology was observed with a transmission electron microscope (TEM), but ceramic structure – with a scanning electron microscope (SEM). Crystalline phases were analyzed by X-ray diffraction (XRD).

Sintered specimens were analyzed by the Archimedes density measurement, X-ray diffraction and SEM observation. Hardness (load: 1 kg) and fracture toughness (load: 10 kg) were measured by the Vickers indentation technique (by Evans and Tanaky). Bending strength was determined by the three-point method at the room and at the 1000 °C temperature.

## Results and discussion

The properties of monolithic composites prepared via hot pressing at 1850 °C are summarized in Table 2. Nanopowder of  $\text{Si}_3\text{N}_4\text{-}6\%\text{Y}_2\text{O}_3\text{-}3\%\text{Al}_2\text{O}_3$  is marked with "A", but with "B" - the nanopowder of  $\text{Si}_3\text{N}_4\text{-TiN}$  with addition of 6 wt. %  $\text{Y}_2\text{O}_3$  and 3 wt. %  $\text{Al}_2\text{O}_3$ .

**Table 2.**

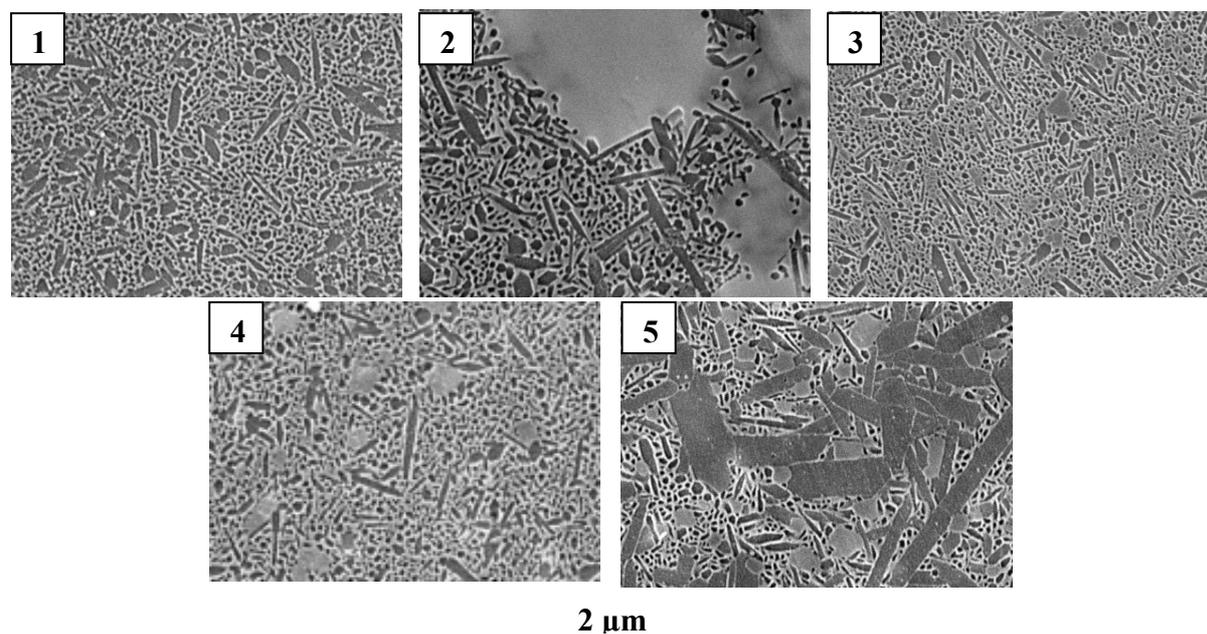
## Properties of monolithic composites

Sample	$\rho$ , g/cm <sup>3</sup>	P <sub>op.</sub> , %	Mechanical properties of sintered body			
			$\sigma_{20}$ , MPa	$\sigma_{1000}$ , MPa	HV <sub>1</sub> , GPa	k <sub>1c</sub> , MPa.m <sup>1/2</sup>
A	3,27	0,1	1052	1020	16,8	5,65
A+10 wt.% ZrO <sub>2</sub>	3,24	0	827	762	15,7	6,11
A+10 wt.% SiC	3,20	0	732	-	17,1	4,97
A+10 wt.% TiN	3,23	0	885	833	15,9	6,00
B	3,22	0,1	976	964	16,9	5,81

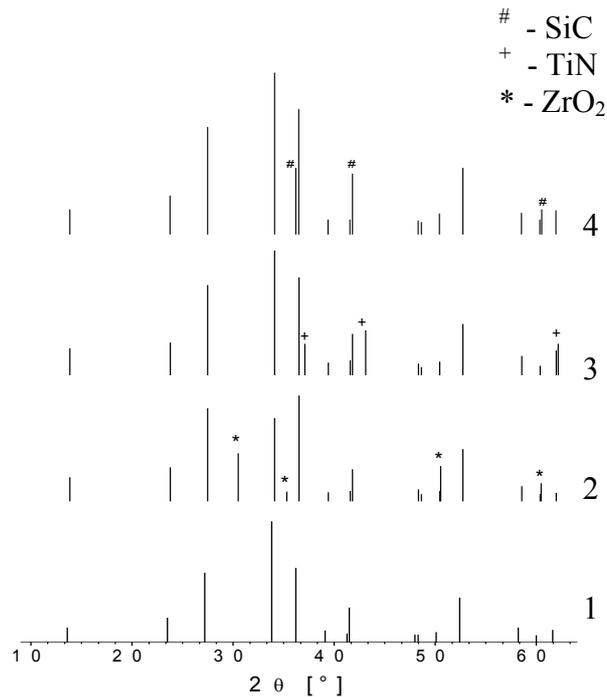
The microstructures of sintered bodies are shown in Fig. 2.

The phase composition of obtained ceramics is given in Fig. 3. The phase analysis of obtained materials shows the presence of  $\beta$ -Si<sub>3</sub>N<sub>4</sub> in all samples as well as the other phase – respectively ZrO<sub>2</sub>,  $\beta$ -SiC and TiN in appropriate samples.

The sintered bodies of the Si<sub>3</sub>N<sub>4</sub>-6Y<sub>2</sub>O<sub>3</sub>-3Al<sub>2</sub>O<sub>3</sub> and Si<sub>3</sub>N<sub>4</sub>-6Y<sub>2</sub>O<sub>3</sub>-3Al<sub>2</sub>O<sub>3</sub> +SiC have maximum density among prepared ceramics. Additives of TiN, ZrO<sub>2</sub> introduced in silicon nitride composites by mechanical mixing decreases the density of Si<sub>3</sub>N<sub>4</sub> based ceramics. Low density (92%) have reached by hot pressing of plasma prepared Si<sub>3</sub>N<sub>4</sub>-TiN composite with oxide additives, possibly due to non-homogeneous mixing of components.



**Fig. 2.** Microstructure of samples A (1), A+10 wt.% ZrO<sub>2</sub> (2), A+10 wt.% SiC (3), A+10 wt.% TiN (4) and B (5).



**Fig. 3.** Phase composition of sintered materials: 1 – sample A ( $\beta$ - $\text{Si}_3\text{N}_4$ ); 2 – A+10%wt.  $\text{ZrO}_2$ ; 3 – A+10%wt. TiN; 4 – A+10wt.% SiC.

The studies of microstructure show that in comparison with the materials prepared at 1800 °C [7], in materials sintered at 1850°C the amount of rod-like crystals and their length increase significantly. The sintered body of synthesized  $\text{Si}_3\text{N}_4$  composite-powder (sample A) exhibited a fine-grained microstructure with small elongated grains. Grains size are mainly of 0,2-0,5  $\mu\text{m}$  and there are a lot of rod-like crystals with the diameter of 0,2-0,4  $\mu\text{m}$  and length of 1,5-3  $\mu\text{m}$  ( $l/d = 4-10$ ).

The same finely grained structure with characteristic rod-like crystals is observed also in the case of ceramics with the  $\text{ZrO}_2$  addition. In this material a separate, homogeneously distributed ball-shaped  $\text{ZrO}_2$  containing inclusions with a size up to 5  $\mu\text{m}$  can be observed.

The samples containing SiC additive have finer microstructure than sample A. It means that SiC inhibits grain growth of  $\text{Si}_3\text{N}_4$ , which agrees with data [8].

More elongated rod-like crystals with the diameter of 0,1-0,5  $\mu\text{m}$  and the length up to 5  $\mu\text{m}$  are observed in silicon nitride ceramics with the additive of TiN. The TiN containing silicon nitride ceramics exhibits a little increased amount at rod-like  $\beta$ - $\text{Si}_3\text{N}_4$  grains in comparison with  $\text{Si}_3\text{N}_4$ -6 $\text{Y}_2\text{O}_3$ -3 $\text{Al}_2\text{O}_3$  ceramics. This observation is consistent with suggestion that fine TiN inclusions works as nuclei accelerating the growth of elongated  $\beta$ - $\text{Si}_3\text{N}_4$  grains [8].

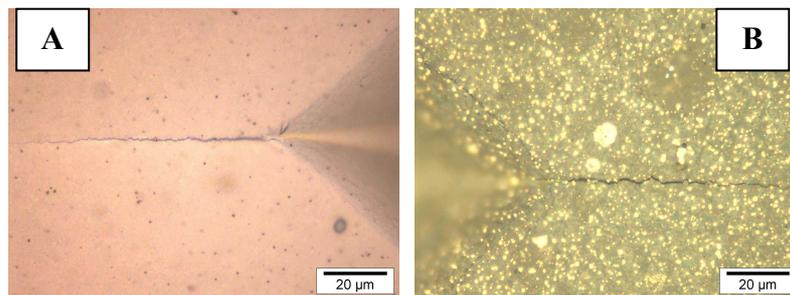
Differing from the mechanical mixture of  $\text{Si}_3\text{N}_4$  and TiN, in the material prepared from  $\text{Si}_3\text{N}_4$ -TiN nanocomposition synthesized in plasma (sample B) there are significantly more such a coarse  $\text{Si}_3\text{N}_4$  grains and they are distributed in matrix from finely grained  $\text{Si}_3\text{N}_4$ .

The increasing of fracture toughness of silicon nitride ceramics with  $\text{ZrO}_2$  additives can be explained by appearing of tensile stresses due to expansion of  $\text{ZrO}_2$  determined by phase transition. The other reason can be the presence of separate coarse grains of  $\text{ZrO}_2$  because it has been proved that the development of some coarse grains in ceramic microstructure can improve the fracture energy [9]. The enhanced fracture toughness of silicon nitride ceramic

with TiN additives can be a result of formation of rod-like  $\beta$ - $\text{Si}_3\text{N}_4$  particles and of appearing of residual stresses caused by different thermal expansion coefficients of  $\text{Si}_3\text{N}_4$  ( $2,8 \times 10^{-6}/^\circ\text{C}$ ) and TiN ( $9,3 \times 10^{-6}/^\circ\text{C}$ ) [10].

The higher value of bending strength, especially at high temperature of sample B in comparison with the sample A+ 10 wt.% TiN prepared by mechanical mixing with similar chemical and phase composition can be explained by more homogeneous distribution of TiN particles in  $\text{Si}_3\text{N}_4$  matrix in plasma prepared composite.

Figure 4 shows the polished surface of samples “A” and “B” with a crack propagated by the Vickers indentation. Cracks are a little bit zigzag-shaped. The zigzagged crack means the crack deflection by rod-like grains contained in this specimen. This is the reason for the increase in fracture toughness.



**Fig. 4.** The polished surface of samples A and B with a crack propagated by the Vickers indentation.

## Conclusions

Evaporation of Si, Ti,  $\text{Al}_2\text{O}_3$ ,  $\text{Y}_2\text{O}_3$  raw powders in radio-frequency nitrogen plasma in the presence of ammonia ensure production of  $\text{Si}_3\text{N}_4\text{-}6\text{Y}_2\text{O}_3\text{-}3\text{Al}_2\text{O}_3$  and  $\text{Si}_3\text{N}_4\text{-TiN}$  nanosized homogeneous composites with average particle size of 35-50 nm.

Bulk materials with fine-grained microstructure and relative density of 92-99 % have been prepared by hot pressing at 1850 °C.

Nanopowder (TiN, SiC,  $\text{ZrO}_2$ ) additives gives the possibility to change the structure and mechanical properties of silicon nitride ceramics.

Mechanical properties of samples obtained after hot pressing at 1850 °C differs from those obtained at 1800 °C with increased mechanical properties and the most significant increase of properties has been observed for  $\text{Si}_3\text{N}_4\text{-}6\text{Y}_2\text{O}_3\text{-}3\text{Al}_2\text{O}_3$  without addition of the second phase.

Due to the complex of properties of prepared materials they could be applied as construction materials for action at high temperatures or probably as wear resistant material, for example, in ball-bearings for acting at the specific conditions (high temperatures, vacuum, without lubricants).

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***N. Zilinska, I. Zālīte, J. Grabis. Uz silīcija nitrīda nanopulveru bāzes ar karsto presēšanu 1850 °c temperatūrā iegūtā keramika.***

*Viens no ceļiem, kā mainīt keramikas materiālu īpašības, ir nanoizmēra izejas pulveru un to kompozīciju pielietošana materiālu ieguvē. Uz silīcija nitrīda bāzes veidotiem materiāliem ir virkne labu īpašību (mehāniskā izturība gan istabas temperatūrā, gan temperatūrās līdz 1400 °C, laba korozijas izturība u.c.), kas nodrošina to praktisku pielietojumu dažādās rūpniecības nozarēs. Pastāv iespēja izmainīt Si<sub>3</sub>N<sub>4</sub> keramikas īpašības ievadot sastāvā otru nanofāzi.*

*Darba mērķis bija noskaidrot otrās fāzes (SiC, ZrO<sub>2</sub>, TiN nanopulveri) ietekmi uz nanokompozīcijas Si<sub>3</sub>N<sub>4</sub>-6%Y<sub>2</sub>O<sub>3</sub>-3%Al<sub>2</sub>O<sub>3</sub> saķepšanu, struktūru un īpašībām, veicot karsto presēšanu 1850 °C temperatūrā.*

*Pētījumi parādīja, ka vairumā gadījumu otrās fāzes piedeva pārveido keramiskā materiāla mikrostruktūru un īpašības.*

***N. Zilinska, I. Zalīte, J. Grabis. Ceramics on the basis of nanodisperse silicon nitride prepared at 1850 °c by hot pressing.***

*One of the ways for modification of ceramic materials properties is application of nanosized compounds and their composites for preparation of materials. Materials based on silicon nitride possess several good properties (mechanical strength both in the room and in the temperatures until 1400 °C, good corrosion resistance and other), ensuring their practical application in different branches of industry. The possibility exists to change the properties of Si<sub>3</sub>N<sub>4</sub> ceramics by addition of a second nanophase.*

*The aim of investigation was to find the effect of the second phase (SiC, ZrO<sub>2</sub>, TiN nanopowders) on sintering, structure and properties of nanocomposite Si<sub>3</sub>N<sub>4</sub>-6%Y<sub>2</sub>O<sub>3</sub>-3%Al<sub>2</sub>O<sub>3</sub> by hot pressing at 1850 °C.*

*It was shown by studies that addition of the second nanophase mostly changes microstructure and properties of material.*

***Н. Жилинска, И. Залите, Я. Грабис. Керамика на основе нанопорошков нитрида кремния, полученная горячим прессованием при 1850 °c.***

*Одним из способов влияния на свойства керамических материалов при их получении является применение исходных нанопорошков и их композиций. Создаваемые на основе нитрида кремния материалы обладают рядом превосходных свойств (механическая прочность при комнатной температуре и температурах до 1400 °C, хорошая коррозионная стойкость и др.), обеспечивающих их*

*применение в различных отраслях промышленности. Существует возможность менять свойства керамики из  $Si_3N_4$  путем ввода в состав дополнительной (второй) нанofазы ( $SiC$ ,  $ZrO_2$ ,  $TiN$ ). Цель представленной работы была выяснить влияние второй фазы на спекание, микроструктуру и свойства материала на основе  $Si_3N_4$ -6% $Y_2O_3$ -3% $Al_2O_3$  при горячем прессовании при 1850 °С. Исследования показали, что в большинстве случаев наличие второй фазы влияет на микроструктуру и свойства керамики.*